

Negative refractive index due to chirality

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We demonstrate experimentally and numerically that metamaterials based on bilayer cross wires give giant optical activity, circular dichroism, and negative refractive index. The presented chiral design offers a much simpler geometry and more efficient way to realize negative refractive index at any frequency. We also developed a retrieval procedure for chiral materials which works successfully for circularly polarized waves.

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Recently, chiral metamaterials are proposed as an alternative to realize negative refractive index.¹⁻³ Chiral metamaterials are metamaterials made of unit cells without symmetry planes. It has been shown that backward waves exist in chiral media.^{1,3} A chiral material slab can focus incident electromagnetic (EM) beams and can be used as a perfect lens.^{4,5} In 2004, the canonical helix³ and the twisted Swiss-rolle metal structures² for microwave applications have been discussed as possible candidates to achieve negative refractive index. Later, the bilayer rosette-shaped chiral metamaterial is proposed and fabricated at microwave frequency^{6,7} and at optical regime.⁸⁻¹⁰ This metamaterial exhibits a very strong rotary power in the microwave, near-infrared, and visible spectral ranges. In the microwave spectral region, in terms of rotary power per wavelength, the bilayer structure rotates 5 orders of magnitude stronger than a gyrotropic crystal of quartz.⁶ It has been shown that the strong gyrotropy originates from the magnetic resonance of the bilayer metallic structure with antiparallel current flowing in the bilayer metal wires.¹¹ In this sense, the bilayer chiral structure is the chiral version of the short wire pair¹²⁻¹⁴ type of metamaterials. The planar chiral structure^{15,16} and chiral photonic crystal¹⁷ are proposed and fabricated. More recently, a chiral split-ring resonators (SRRs) design consisting of double layers of SRRs is proposed to provide negative refractive index.¹⁸

In this Rapid Communication we demonstrate, experimentally and numerically, the negative refraction using the bilayer cross-wire design. We show the negative refraction originates from the three-dimensional chiral properties of the bilayer cross wires. Unlike conventional negative index material designs, such as the split-ring resonator type design¹⁹ and fishnet designs,²⁰ the chiral negative index material does not require simultaneously negative permittivity and permeability, and, therefore, the chiral design can offer much simpler geometry and a more efficient way to realize negative refraction index. Due to the asymmetric geometry of the cross-wire pairs, the cross coupling between the magnetic field and electric field happens at the chiral resonances and provides strong chirality around the resonance frequencies. Further study shows chiral resonances are either electric resonance or magnetic resonance of short wire pairs. The negative refractive index of chiral metamaterial arises from this strong chirality, which splits the refractive indices, n_{\pm} , of

the two circularly polarized waves and makes the refractive index of one circular polarization become negative.² Our study shows that two resonance modes exist for the cross-wire pairs. The resonance mode at the lower frequency is a magnetic resonance mode with antiparallel currents, while the resonance mode at the higher frequency is an electric resonance with parallel currents.

We develop a retrieval procedure adopting the uniaxial bianisotropic model to calculate the effective parameters, μ , ϵ , κ and n_{\pm} , of the chiral metamaterial design. We prove the existence of the negative index originating from the chirality κ of the cross-wire metamaterial. As a comparison, the non-chiral version of the cross-wires pair design does not show any negative refractive index. Finally, we study the current distribution for both the electric and the magnetic resonances, and determine electric and magnetic resonances are the symmetric and antisymmetric resonance modes of the coupled short wire resonances, respectively.

The layout of the proposed structure is shown in Fig. 1. An 18×14 array of cross wires is patterned on a double side copper-clad FR-4 board. The overall size of our sample is 279×216 mm². The dielectric constant of the FR-4 board is $\epsilon_r = 4.5 + 0.15i$. The properties of the cross wires shown in Fig. 1 are characterized, using simulations and microwave measurements, and these results are used to determine the expected properties of metamaterials built from the cross-wire building blocks. Simulations of cross-wire structures are achieved with CST Microwave Studio (Computer Simu-

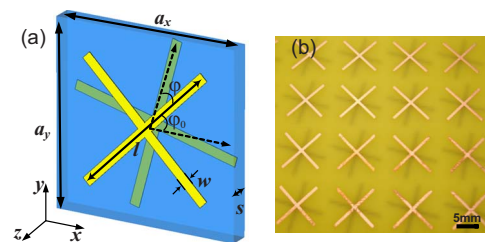


FIG. 1. (Color online) (a) Schematic representation of one unit cell of the cross-wire structure. (b) Photograph of one side of a fabricated microwave-scale cross-wire sample. The geometry parameters are given by $a_x = a_y = 15$ mm, $l = 14$ mm, $w = 0.8$ mm, $s = 1.6$ mm, $\phi_0 = 45^\circ$, and $\phi = 30^\circ$. The thickness of the copper is $t_m = 36$ μ m.

lation Technology GmbH, Darmstadt, Germany), which uses a finite element method to determine reflection and transmission properties. In the simulations, the periodic boundary conditions are applied to a single unit cell shown in Fig. 1(a). Since the eigensolutions of the EM wave in chiral materials are two circularly polarized EM waves,^{21,22} i.e., the right-handed circularly polarized wave (RCP, +) and the left-handed circularly polarized wave (LCP, -), correspondingly, four transmission coefficients,²³ T_{++} , T_{-+} , T_{+-} , and T_{--} , are

$$\begin{pmatrix} T_{++} & T_{+-} \\ T_{-+} & T_{--} \end{pmatrix} = \frac{1}{2} \times \begin{pmatrix} (T_{xx} + T_{yy}) + i(T_{xy} - T_{yx}) & (T_{xx} - T_{yy}) - i(T_{xy} + T_{yx}) \\ (T_{xx} - T_{yy}) + i(T_{xy} + T_{yx}) & (T_{xx} + T_{yy}) - i(T_{xy} - T_{yx}) \end{pmatrix}. \quad (1)$$

Figures 2(a) and 2(b) show the simulated and measured transmission coefficients, T_{++} and T_{--} , as a function of frequency, respectively (the cross coupling transmission, T_{-+} and T_{+-} , are negligible, not shown here). Due to the asymmetric geometry along the propagating direction, the transmission responses for RCP and LCP split into two curves. Notice two resonance dips are observed at frequencies,

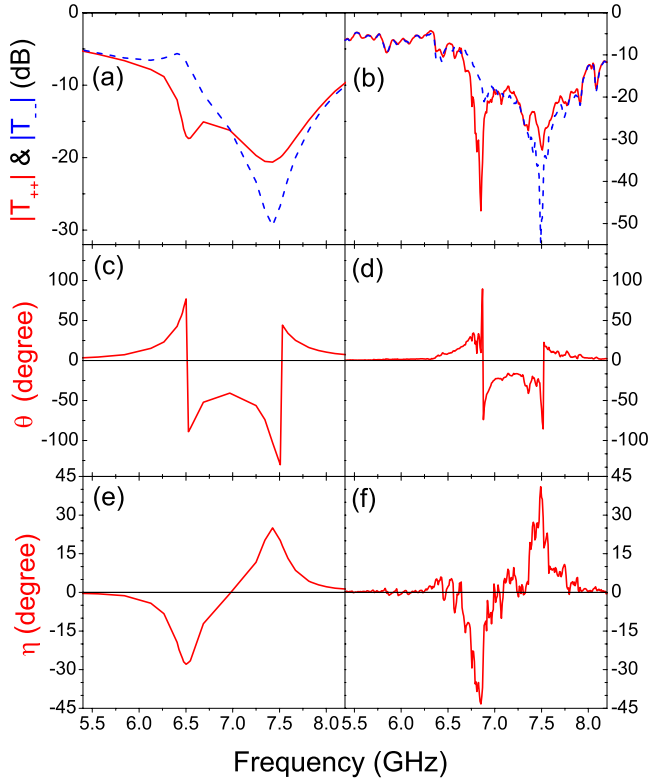


FIG. 2. (Color online) (a) and (b): Simulated and measured magnitude of the transmission coefficients for the right circularly polarized, $|T_{++}|$ (red solid), and the left circularly polarized, $|T_{--}|$ (blue/dark gray dashed), electromagnetic wave, respectively. (c) and (d): Simulated and measured polarization azimuth rotation, θ , respectively. (e) and (f): Simulated and measured ellipticity angle, η , respectively.

obtained to fully characterize the response of the chiral metamaterials. In the experiment, the transmission coefficient is measured by HP 8364B network analyzer with two Narda standard horn antennas. Four linear transmission coefficients, T_{xx} , T_{yx} , T_{xy} , and T_{yy} , are measured and the circular transmission coefficients, T_{++} , T_{-+} , T_{+-} , and T_{--} are converted from the linear transmission coefficients using the following equation:

$f=6.5$ and 7.5 GHz, in both T_{++} and T_{--} curves. For the first resonance at 6.5 GHz, the transmission dip for RCP, T_{++} , is much deeper than that for LCP, T_{--} , which implies the resonance for RCP is much stronger than LCP. While, for the second resonance at 7.5 GHz, we observe the resonance for LCP is much stronger than RCP. Using the standard definitions²⁴ of the polarization azimuth rotation, $\theta = [\arg(T_{++}) - \arg(T_{--})]/2$, and the ellipticity, $\eta = \frac{1}{2} \arcsin\left(\frac{|T_{++}| - |T_{--}|}{|T_{++}| + |T_{--}|}\right)$, of elliptically polarized light, we calculate the polarization changes in a linearly polarized wave incident on the cross-wire structures. The simulated and measured azimuth rotation, θ , and ellipticity, η , are presented in Figs. 2(c) and 2(e) and Figs. 2(d) and 2(f), respectively. At the resonance frequencies of 6.5 and 7.5 GHz, the azimuth rotation and ellipticity reach their maximum values, $(\theta = -89^\circ, \eta = -28^\circ)$ and $(\theta = -130^\circ, \eta = 28^\circ)$, respectively. In the region between two resonance dips (around 6.9 GHz), the region with low loss and nearly zero dichroism, we observe a polarization rotation of -40° with $\eta \approx 0$, about four times larger than the value reported using similar bilayer chiral metamaterial designs, such as bilayer of twisted rosettes.^{6,7} The sign change of η at 7.0 GHz reflects the different frequency dependence between the magnitude of the transmission $|T_{++}|$ and $|T_{--}|$. As a consequence, the outgoing wave of a linear polarized incident wave below and above 7.0 GHz have different handedness. Our numerical simulations show that the differences between $|T_{++}|$ and $|T_{--}|$ result from the different amounts of loss as the RCP and LCP waves pass through the cross-wire structures.

To study the effective parameters of chiral metamaterials, we develop a retrieval procedure based on a uniaxial bianisotropic model.⁷ The cross-wire pairs design can be modeled as a reciprocal uniaxial bianisotropic medium and the constitutive equation is given by

$$\begin{pmatrix} \mathbf{D} \\ \mathbf{B} \end{pmatrix} = \begin{pmatrix} \epsilon_0 \epsilon & i\kappa/c_0 \\ -i\kappa/c_0 & \mu_0 \mu \end{pmatrix} \begin{pmatrix} \mathbf{E} \\ \mathbf{H} \end{pmatrix}, \quad (2)$$

where ϵ_0 , μ_0 , and c_0 are the permittivity, permeability, and the speed of light in a vacuum, respectively. Assuming $\exp(-i\omega t)$ time dependent, the eigensolution of the electro-

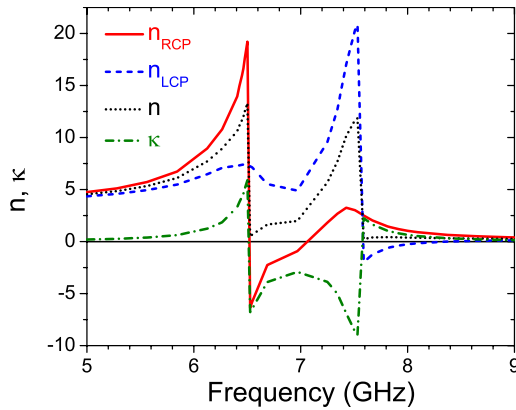


FIG. 3. (Color online) The retrieved effective refractive index for the right circularly polarized EM wave, n_+ (red/gray solid), and the left circularly polarized EM wave, n_- (blue/dark gray dashed). The black dotted curve shows the refractive index calculated by the permittivity and the permeability, $n = \sqrt{\epsilon\mu}$, and the green/light gray dash-dotted curve shows the chiral parameter, κ .

magnetic wave in bi-isotropic media is circular polarized plane waves, and the polarization is either LCP or RCP. The refractive indices for LCP and RCP are given by^{21,22}

$$n_{\pm} = \sqrt{\epsilon\mu} \pm \kappa, \quad (3)$$

where (+) and (−) denote RCP and LCP, respectively. Both LCP and RCP have the same impedance given by $z/z_0 = \sqrt{\mu/\epsilon}$, where z_0 is the impedance of the vacuum.

From Eq. (3), one can immediately see that $n < 0$ for one of the polarizations, if κ is large enough, such that $\sqrt{\epsilon\mu} < \kappa$. It has been shown that the polarization azimuth rotation, θ , is proportional to the chiral parameter, κ . Specifically, $\theta = \kappa k_0 d$, where k_0 and d are the wave vectors in a vacuum and the thickness of the bi-isotropic slab. Thus, the chiral materials with large rotary power, such as the bilayer structures and chiral SRRs, possibly possess the negative refractive index. However, it is not trivial to obtain negative refractive index by a chiral design with a large azimuth rotation. One should keep in mind that the large value of azimuth angle, θ , happens at the resonances, where $\sqrt{\epsilon\mu}$ is also large, so κ should be large enough to overcome the large magnitude of $\sqrt{\epsilon\mu}$ to achieve negative n .

In Fig. 3, we present the refractive index for RCP and LCP, n_+ , n_- , the conventional definition of refraction index, $n = \sqrt{\epsilon\mu}$, and the chiral parameter, κ , which are extracted from simulation results using the retrieval procedure. A thickness, $d = s + 2t_m = 1.672$ mm, is used when we extract these effective parameters. Notice that n (black dotted curve) is positive through the entire frequency range from 5 to 9 GHz. However, n_+ (red solid) is negative from 6.5 to 7.0 GHz and n_- (blue dashed) has a negative region from 7.6 to 8.2 GHz. The chiral parameter (green dash-dotted curve) shows two resonances at 6.5 and 7.5 GHz, respectively. Above the first resonance frequency, κ is negative between 6.5 to 7.0 GHz, which leads to $n_+ = \sqrt{\epsilon\mu} + \kappa < 0$ between 6.5 to 7.0 GHz. Similarly, above the second resonance frequency, κ is positive and results in $n_- = \sqrt{\epsilon\mu} - \kappa < 0$ between

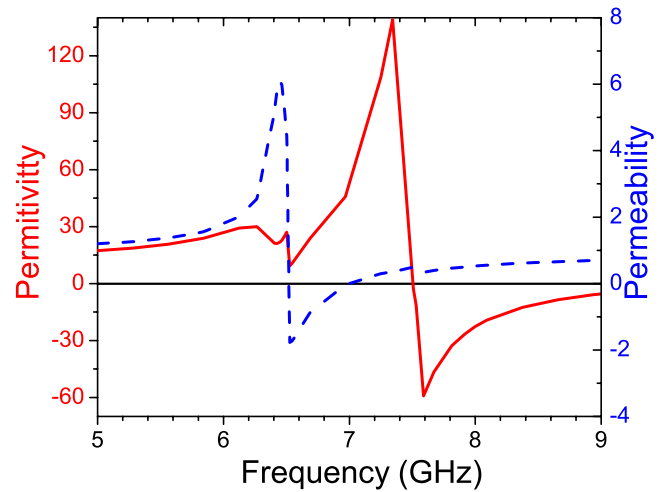


FIG. 4. (Color online) The real part of the effective permittivity (red/gray solid) and the effective permeability (blue/dark gray dashed), extracted from the simulation data.

7.6 to 8.2 GHz. It is clear the negative refractive index for RCP and LCP originates from the chiral parameter, κ . The observed negative refractive index $n_+ = -2.5$ at 6.8 GHz has the figure of merit, $\text{FOM} = |\text{Re}(n)/\text{Im}(n)| = 0.75$, and $n_- = -1$ at 7.8 GHz has $\text{FOM} = 0.5$. The figure of merit is relatively low compared to the conventional negative index material designs such as SRRs or fishnet. The low FOM is due to the high loss of this chiral metamaterial design. Further study shows the loss mainly originates from the lossy dielectric spacer. If low loss dielectric materials are used in the cross-wire design, the FOM can improve substantially. For instance, in our numerical simulations, we obtained $\text{FOM} \approx 10$ using dielectric spacer with $\epsilon_r = 4.5 + 0.005i$.

We also calculate the n_+ , n_- , n , and κ for a nonchiral cross-wire pairs with the mutual twisted angle $\phi = 0$. The results show $n_+ = n_- = n > 0$, and the chiral parameters, $\kappa = 0$ through the entire frequency range from 5 to 9.0 GHz. Thus, we confirm the negative refractive index observed in Fig. 3 is due to the chirality introduced by the asymmetry of the cross-wire pairs.

In Fig. 4, we present the real parts of the permittivity, ϵ , and the permeability, μ , as a function of frequency for the asymmetric cross-wire pairs. Two resonances are observed in μ (blue dashed) at 6.5 and ϵ (red solid) at 7.5 GHz, respectively. This demonstrates the resonance observed in Figs. 2 and 3 at 6.5 GHz is a magnetic resonance and the resonance at 7.5 GHz is an electric resonance. The magnetic resonance gives the negative μ between 6.5 to 6.9 GHz, and the electric resonance give a negative ϵ between 7.6 to 9 GHz. There is no overlap region of negative ϵ and μ . Therefore, $\text{Re}(n) = \text{Re}(\sqrt{\epsilon\mu}) > 0$, which is consistent with the observation of $\text{Re}(n) > 0$ shown in Fig. 3.

In order to understand the mechanism of the resonances for the cross-wire pair design, we studied the current density distribution as shown in Fig. 5. Notice, at the magnetic resonance, the antiparallel current exists on the top and bottom layer of cross-wire pairs [Fig. 5(a)], which is an asymmetric resonance mode. In Fig. 5(b), one can see parallel currents flowing on the two layers of wires, which is a symmetric

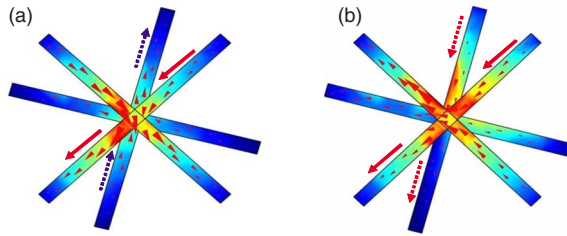


FIG. 5. (Color online) The simulated current density distribution for the right circularly polarized EM wave at 6.5 GHz (a) and for the left circularly polarized EM wave at 7.5 GHz (b). The cones (in red) show the direction and magnitude of the current density. The magnitude of the current density is also shown by the color on the wires, with red and blue corresponding to largest and smallest values.

resonance mode. The current distribution shows that the cross-wire pairs can be viewed as a chiral version of the short wire pairs,^{12–14} which has similar current distributions in the symmetric and asymmetric resonance modes.

In summary, we experimentally demonstrated bilayer cross wires with very adaptable properties, including negative index of refraction due to chirality, giant optical activity,

and very large circular dichroism. We performed numerical simulations that give evidence that the negative refractive index is due to the chiral nature of the metamaterial and not from the simultaneous negative ϵ and μ as for conventional negative index materials. In addition, we developed a retrieval procedure that works well for chiral metamaterials. The geometry of the cross-wire design is simple and easy to fabricate, and therefore, is more suitable for optical frequency applications compared to other types of bilayer chiral metamaterial designs.

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